

Design of Two Speed Gearbox for CNC Lathe

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ABSTRACT

Since gearboxes in lathe are positioned inside the headstock, an aftereffect of vibration is experienced in the spindle and further leads to inaccuracy in the finished products, also causes inconveniences during the maintenance and also increases difficulties if any replacements are needed. In a complex work the accuracy plays a major role and hence the above problems are to be eliminated accordingly.

This project aims to design a gearbox which can be placed outside the headstock and also aims to design in such a way that a single base is utilized for Lathe and new gearbox.

Key Words: Gears, Gearbox, CNC, Lathe, Direct Drive, Power Transmission

I. INTRODUCTION

Gearboxes provide for a wide range of cutting speeds and torque from a constant speed power input enabling proper cutting speeds or torque to be obtained at the spindles as required in the case of cutting drives and desired feed rates in the case of feed drives. The design of gearbox is intimately linked with the whole structure of the spindle drives. The gearbox can be built integral into the spindle head housing. This type of arrangement promotes more compact spindle drives, higher localization of controls, fewer housings and less assembly work involving in the fitting of joining surfaces.

Main drawback is the possibility of transmitting vibration from the gearbox to the spindle, heating of the spindle head by the heat generated in the gearbox.

The gear box can also be arranged in separate housing and linked to the spindle head through belt transmission. This type of arrangement has advantage that neither the heat generated by neither frictional losses nor vibrations developed in the gearbox are transmitted to the spindle head.

1.1 Indirect Drive

Design of gearbox mainly depends upon the tool workpiece combinations used. Here we are using

aluminium whose cutting speed varies from 188 rpm to 3000 rpm. Motor is selected which is working under a speed range equal to 1500 rpm to 6000 rpm. While selecting motor power ratings should be kept to minimum value in order to maintain low economy of lathe. From SIEMENS motor catalogue, motor selected is "SIEMENS" squirrel cage induction standard three phase motor" – 1PH8087. Its specifications are given below

- Rated power – 3.7KW
- Rated speed – 1500rpm
- Rated current – 10A
- Rated voltage – 400V

Since we are designing two speed gearbox it is possible for obtaining two different rpms from an input motor rpm.

stages we could get a lower rpm of 188 to a higher rpm of 3000 with the maximum torque/ power. Designing a ray diagram is necessary for finding out speed ratios between rotor shaft of motor and driver shaft of gearbox, driver shaft and driven shaft, driven shaft and output shaft. Procedure for drawing ray diagram is given in the next section.

1.2 Disadvantages of Existing System

The indirect drive involved power transmission through gears throughout the entire speed range of the motor. This results in power loss in the form of frictional losses in the gears. When the speed requirement for cutting comes in the constant power range of the motor power transmission can be directly to the spindle thereby transmission loss through gears can be avoided in these speed ranges. Hence a new gearbox design was developed incorporating a clutch which bypasses transmission through gears for the constant power speed range of the motor.

II. DESIGN OF INDIRECT DRIVE (Using Gears)

2.1. Ray Diagram

The speed chart or ray diagram is a graphical representation of the drive arrangement in the general form. In other words, the ray diagram is a graphical representation of the structural formula.

A ray diagram can be used to easily explain the speed reduction stages. Motor – gear box stage is the first V-belt stage. V-belt pulley assembly is used to provide a speed ratio of 1:2. Second stage is gear box stage. Here two gear ratios are provided to give the required speed range. The last stage is another V-belt stage with a speed ratio 1:2.

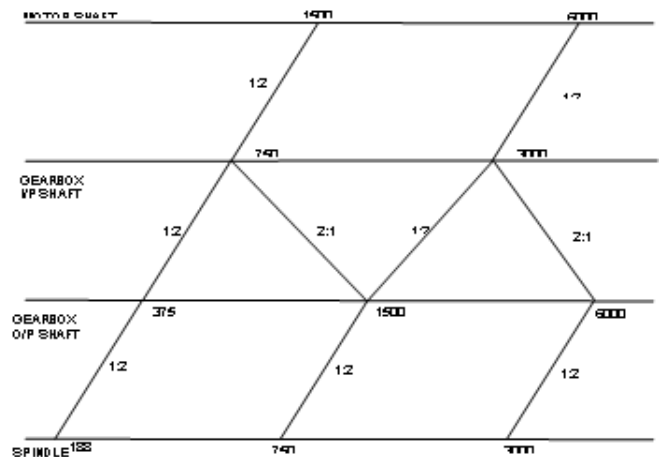


Fig.2.1.1 Ray Diagram

All these stages help to get a speed range between 188 RPM to 3000 RPM with a constant power from the induction motor. The diametrical changes of the pulley initiate the first speed reduction. The next speed reduction in the gears depends upon the gear ratio. The gear ratios are fixed to attain the required rpm in the lathe. Thus, by these three reduction stages we could get a lower rpm of 188 to a higher rpm of 3000 with the maximum torque/ power.

2.2. Design of indirect drive system (Using gears)

The whole assembly design of the gearbox consists of the gear pairs, input and output shaft, shaft bearings. Also, the design of the V-belt drive should be done to complete the full driving mechanism from motor to the spindle.

A 3D model of gear pairs, belt-pulley system and gearbox created using modeling software Solidworks is presented in figures given below.

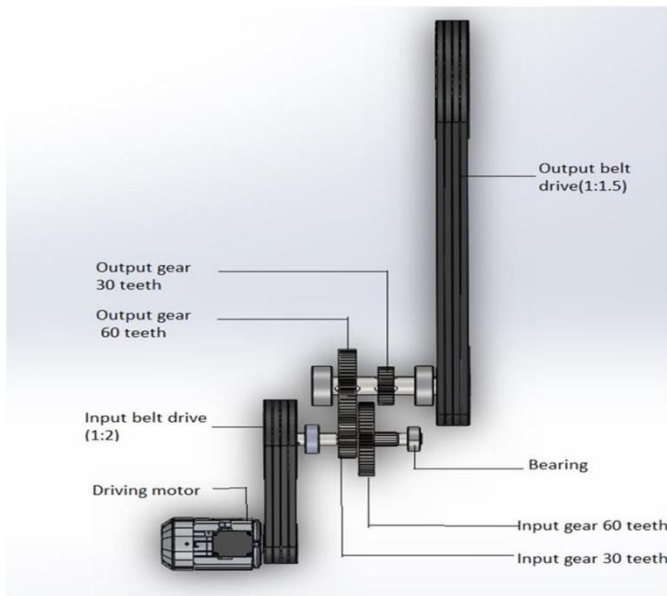


Fig.2.2.1 Top view of the gearbox



Fig.2.2.2 3D Model of the gearbox

2.3. Design of indirect drive system (Using clutch)

When the speed requirement for cutting comes in the constant power range of the motor power transmission can be directly to the spindle. Also, transmission loss through gears can be avoided in these speed ranges. Hence a new gearbox design was developed incorporating a clutch. The clutch used is single plate dry friction clutch. This is a new design which is not currently in use.

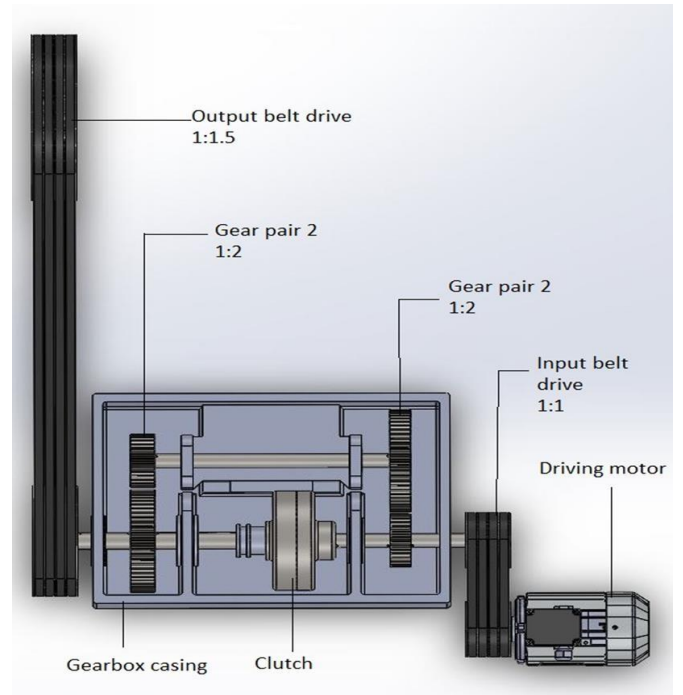


Fig. 2.3.1 Top View



Fig. 2.3.2 Isometric View

III. RESULTS

Here, we conclude that our design was successfully generated with the help of the software SolidWorks and the design is okay to proceed for the desired CNC lathe with the effect of the reduced vibration and in accordance with no increase in the base or space requirements of the initial machine (CNC Lathe). Thus we conclude that our design study was a success.

| SL.NO | PORTIONS | INPUT | OUTPUT |
|-------|------------------------------|--|--|
| 1 | PITCH CIRCLE DIAMETER | | |
| | •Z = 30 & 60 •Z = 60 & 30 | D1 = 90mm D1 = 180 mm | D2 = 180 mm D2 = 90 mm |
| 2 | No: of teeth | Z1 = 30 Z2 = 60 | Z1 = 60 Z2 = 30 |
| 3 | BELTS | Motor to gear | Gear to spindle |
| | LENGTH | Nominal pitch length= 1102mm Nominal inside length = 1067mm | Nominal pitch length= 3084mm Nominal inside length = 3048mm |
| | CENTRE DISTANCE | C = 286.5 mm | C = 1066.06 mm |

| Sl.no | PORTIONS | INPUT | OUTPUT |
|-------|-------------------------|--|--|
| | No: of belts | N = 4 | N = 4 |
| 4 | PULLEY | | |
| | Diameter | D1 = 220mm | D2 = 200mm |
| | Tension acting in belts | T1 = 236.26 N T2 = 22.02 N | T1 = 1020.38 N T2 = 77.95 mm |
| 5 | SHAFT | | |
| | Diameter | D = 20mm (for z1 = 30) D = 25mm (for z2 = 60) | D = 25mm (for z1 = 60) D = 20mm (for z2 = 30) |
| | Width | B = 12mm A = 34.9 mm | A = 23mm B = 86.3mm |

| Sl.no | PORTIONS | INPUT | OUTPUT |
|-------|----------------|---|---|
| | Inner diameter | B = 17mm A = 35mm | A = 50mm B = 80mm |
| | Outer diameter | B = 40mm A = 80mm | A = 90mm B = 170mm |
| 7 | BEARINGS | INPUT SHAFT B Life = 4500 hrs Load = 4608.64 N Type = single row angular contact ball bearing (17BA02) | OUTPUT SHAFT A Life = 9000 hrs Load = 43340 N Type = cylindrical roller bearing (NU2210) |
| | | INPUT SHAFT A Life = 4500 hrs Load = 42537.01 N Type = double row angular ball bearing (3307A) | OUTOUT SHAFT B Life = 9000 hrs Load = 141261.57 N Type = double row angular contact ball bearing (3316A) |

| Sl.no | PORTIONS | INPUT | OUTPUT |
|-------|----------------|---|---|
| | | INPUT SHAFT A Life = 4500 hrs Load = 42537.01 N Type = double row angular ball bearing (3307A) | OUTOUT SHAFT B Life = 9000 hrs Load = 141261.57 N Type = double row angular contact ball bearing (3316A) |
| 8 | KEYS | | |
| | Size (b x h) | 8mm x 7mm | 8mm x 7mm |

Table 3.1 : Design calculation results

IV. APPLICATIONS

- Extremely compact design.
- High accuracy and high-power density in a minimal space.
- Coaxial design. Gearbox integrated in-line between a water-cooled motor and a spindle inside a RAM.
- Large output bearings provide high tilt capacity.
- A large hollow shaft, that goes through the system, to facilitate the installation of hydraulic draw bar and spindle coolant system.
- Smoother motion due to optimized Servotak gears.
- Better performance compared to conventional two speed gearboxes.
- The low noise shift mechanism meets strict machine tool requirements.
- The actuator used for the speed change is integrated into the gearbox design.
- High speed for soft materials and high torque for hogging out steel or hard materials.
- Increased production rates thanks to high speed gears.
- Greatly reduced the cycling times.

V. CONCLUSION

The design of two speed variable speed gearbox for the headstock of CNC lathe as per the requirement has done successfully. The different speed ratios are now made available with this gearbox. The works which require lower rpm can be done easily without any trouble. The design is mainly based on consideration like compactness, longer service life with minimum breakdown periods. Gearbox uses existing casting of the mother machine. Since the gearbox is fixed on the machine casting itself, there is no need of separate base. Thus no extra floor space is needed. Less power motor is employed for supplying high torque. Also the designed gearbox is small yet efficient, durable, reliable and provides sufficient torque. If the size of the gearbox is not a design consideration, an intermediate shaft can be employed for effective power transmission. This eliminates overhanging gear on motor shaft. Speed increasing drives are not commonly used in gearbox of machine tools. It can be replaced with a reduction gear of suitable gear ratio. The economic viability of design can be increased

while choosing factor of safety for each component. However, choosing an optimum factor of safety development in material science and manufacturing technology, new materials with greater design stresses and reduced stress concentration and precision machined will be available. These results in a more compact, safe and economical design suitable for industries.

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