

Comparative Study on Overturning Moment and Eccentricity of A I-Shaped Building by Equivalent Lateral Force and Modal Response Spectrum Method Using ETABS Software M. T. Hasan^{*1}, M. L. Hossain²

¹Workshop Maintenance Engineer, Department of Civil Engineering, Sylhet Engineering College, Sylhet, Bangladesh

²Structural Design Engineer, Bismillah Engineering and consultancy, Sirajganj, Bangladesh

ABSTRACT

Article Info

Volume 8, Issue 4 Page Number : 173-179

Publication Issue July-August-2021

Article History

Accepted : 02 July 2021 Published : 09 July 2021 Extended Three-Dimensional Analysis of Building System (ETABS) (version19) is a powerful software, used for building analysis and design. This software used for analysis purpose to this study. The study in this paper mainly strengthens on overturning moment and eccentricity of I-shaped fifteen storied building in both equivalent lateral force method and modal response spectrum method. The analyses are carried out as per ASCE7-16 and BNBC 2020 guidelines. It is observed that the overturning moment is approximately 11% greater in equivalent lateral force method than modal response spectrum method while in eccentricity approximately 2% greater in modal response spectrum method than equivalent lateral force method.

Keywords : ETABS, Analysis, Overturning moment, eccentricity, equivalent lateral fore method, modal response spectrum method.

I. INTRODUCTION

Lateral loads or earthquake loads are more sensitive to high-rise building. But when the eccentricity between mass centre and stiffness centre more the building induce irregularity and more vulnerable to seismic hazard [1]. The eccentricity depends on mass distribution and stiffness of each story on which centre of mass positioned. Due to eccentricity torsional effect induced. When earthquake shaking produce this torsional effect is more dangerous to building stability [2].

Building subjected to earthquake loading produce shear force in each story of building. These forces are produces overturning moment of the building. For rectangular regular shape building is less susceptible to overturning moment than I-shaped building.

The objectives of this work to study the eccentricity and overturning moment of I-shaped building in both equivalent lateral force method and modal response spectrum method.

II. METHODS AND MATERIAL

This work is based on software. A software name Extended Three-Dimensional Analysis of Building System (ETABS) version 19 used for this study. 15 (fifteen) storied residential building of I-shaped

Copyright: © the author(s), publisher and licensee Technoscience Academy. This is an open-access article distributed under the terms of the Creative Commons Attribution Non-Commercial License, which permits unrestricted non-commercial use, distribution, and reproduction in any medium, provided the original work is properly cited



considered to study eccentricity and overturning moment. Equivalent Lateral Force Method and Modal Response Spectrum Analysis were used to perform for analysis. At first Equivalent Lateral Force Method was performed and then Modal Response Spectrum Analysis was performed. In analysis the materials properties considered as tabulated in table 2.1. The section properties tabulated in table 2.2. The load case and load combination tabulated in 2.3 and 2.4 respectively. For modal response spectrum analysis, the modes were selected 3 (three) times the number of stories. 2D plan, beam information, column information, shear wall position shown in figure 2.1, 2.2, 2.3, 2.4 respectively. Also, 3D view shown in figure 2.5.

Table 2.1: materials properties

| Material type | Strength |
|------------------------------------|----------|
| Concrete for column and shear wall | 3500 psi |
| Concrete for beam and slab | 3000 psi |
| Rebar | 60 grade |

Table 2.2: section properties

| | 1 1 |
|--------------------|---------|
| Туре | Size |
| Column 1 (C1) | 12"x25" |
| Column 2 (C1) | 12"x27" |
| Column 3 (C1) | 14"x30" |
| Column 5 (C1) | 12"x18" |
| Floor beam (B1-B5) | 10"x24" |
| Grade beam | 12"x24" |
| Shear wall | 10" |
| Slab (shell thin) | 5.5'' |
| | |

Table 2.3: load cases

| Table 2.5. Ioad cases | | | | |
|-----------------------|-------------------|--|--|--|
| Name | Туре | | | |
| Dead | Linear Static | | | |
| Modal | Modal - Ritz | | | |
| WALL | Linear Static | | | |
| PW | Linear Static | | | |
| FF | Linear Static | | | |
| LIVE | Linear Static | | | |
| HOSPITAL LIVE | Linear Static | | | |
| STAIR LIVE | Linear Static | | | |
| ROOF LIVE | Linear Static | | | |
| LIFT DL | Linear Static | | | |
| LIFT LL | Linear Static | | | |
| OHWT | Linear Static | | | |
| EQX | Linear Static | | | |
| EQY | Linear Static | | | |
| WX | Linear Static | | | |
| WY | Linear Static | | | |
| RSX | Response spectrum | | | |
| RSY | Response spectrum | | | |
| | · | | | |

Table 2.4: Basic load combination

| 1.4D |
|------------------|
| 1.2D+1.6L |
| 1.2D+1.0L |
| 1.2D+1.6W+1.0L |
| 1.2D+1.0 E+1.0 L |
| 0.9D+1.6W |
| 0.9D+1.0 E |

Loads acting on the structure are dead load (DL), live load (LL), earthquake load, wind load. Self-weight consists of the weight of beam, column, slab and shear wall of the building. Wall Loads are Super Imposed Dead Load (SIDL). These loads are the loads of the brick walls which are located on the beams. Wall loads are calculated as per linear foot and applied on the model simultaneously as per wall positions.in this study wall load 0.5k/ft applied. Partition Wall Loads are also Super Imposed Dead Load (SIDL). This load are the loads of the brick walls which are located on the slab panels. Partition wall loads are calculated as per square foot and applied on the model simultaneously as per wall positions. In this study 75psf applied Floor Finish Loads are also Super Imposed Dead Load (SIDL). These loads are the loads of the tiles, plasters on the slab panels. Floor finish loads are calculated assuming unit weight 145 pcf. and thickness of floor finish 1.5 inch.

Floor finish= $1.5inX (145pcf) = 18.125 psf. \approx 20 psf.$ For Lift machine Load's shaft size Assumed 5'-4"X4'-8". From Public Works Department schedule, total load=8 tons = 17600lb. Machine room floor area= 7'X6'=42 sq.ft. So, total lift machine load = 176000/42= 419.05 psf. Portion of total load assumed as Dead load = 50% of total load= 209.52 psf. Portion of total load assumed as Live load = 50% of total load= 209.52 psf. Floor live load and roof live loads are applied separately on each floor and top of the floor. Stair live load applied in stair slab. Live load on the residential floor slabs = 42 psf. Live load on the roof slab = 100psf. Live load on the stair = 100 psf. Live load for hospital floors=100 psf. Wind load are applied in X and Y direction as per BNBC 2020, PART 6, Chapter 2. For seismic load: soil type: SC, Importance factor: 1, Response reduction factor:7, Damping: 5%, seismic zone: III as per BNBC 2020, PART 6, Chapter 2 [3].



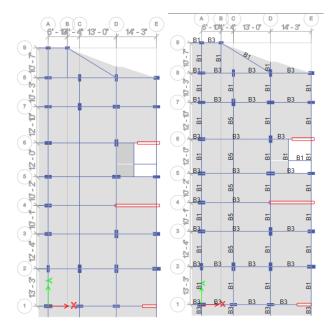


Fig.2.1 Plan of building Fig.2.2 Beam information

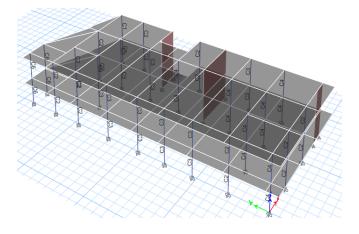


Fig2.3 Column information

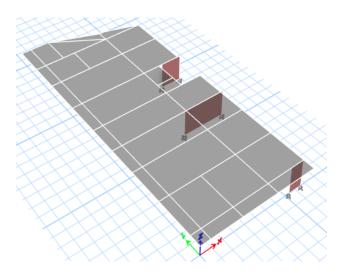


Fig2.4 Shear wall position

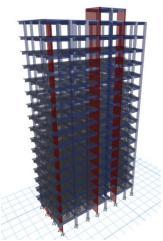


Fig.2.5 3D view of the building

III.RESULTS AND DISCUSSION

After completing the model, static force method and modal response analysis were running. The structure shall be designed to resist overturning effects caused by the seismic forces. At any story, the increment of overturning moment in the story under consideration shall be distributed to the various vertical force resisting elements in the same proportion as the distribution of the horizontal shears to those elements. The overturning moments at level x, Mx determined as follows:

$$M_x = \sum_{i=x}^n F_i(h_i - h_x)$$
(3.1)

where,

Fi= Portion of the seismic base shear, V

induced at level i

 h_i , h_x = Height from the base to level i or x.

Overturning moment for earthquake load for equivalent lateral force method in x direction was found as 63718 kip-ft which calculation shown in the table 3.1, where in modal response spectrum analysis was found as 56308 kip-ft. shown in table 3.2. In Y direction overturning moment was found as 63318 kip-ft in equivalent lateral force method shown in table 3.3 where in response spectrum analysis was found as 56442 kip-ft shown in table 3.4. Table3.1: The calculation of overturning moment for earthquake load in x direction in equivalent lateral force method

| Level | Story Ht | Elev | ETAB S Cum. Story Force/ Shear (Vx) | Individual Story Force/ Shear (Vx) | Overturning Moment (OM) |
|----------|-------------|------|---|--|----------------------------|
| ROO F | 10 | 160 | 58.641 | 58.641 | 9382.56 |
| F14 | 10 | 150 | 128.14 1 | 69.5 | 11120 |
| F13 | 10 | 140 | 190.72 2 | 62.581 | 9387.15 |
| F12 | 10 | 130 | 246.63 6 | 55.914 | 7827.96 |
| F11 | 10 | 120 | 296.14 5 | 49.509 | 6436.17 |
| F10 | 10 | 110 | 339.52 | 43.375 | 5205 |
| F9 | 10 | 100 | 377.04 6 | 37.526 | 4127.86 |
| F8 | 10 | 90 | 409.01 8 | 31.972 | 3197.2 |
| F7 | 10 | 80 | 435.75 | 26.732 | 2405.88 |
| F6 | 10 | 70 | 457.57 1 | 21.821 | 1745.68 |
| F5 | 10 | 60 | 474.83 4 | 17.263 | 1208.41 |
| F4 | 10 | 50 | 487.91 8 | 13.084 | 785.04 |
| F3 | 10 | 40 | 497.23 9 | 9.321 | 466.05 |
| F2 | 10 | 30 | 504.29 6 | 7.057 | 282.28 |
| F1 | 10 | 20 | 508.10 2 | 3.806 | 114.18 |
| GF | 10 | 10 | 509.45 2 | 1.35 | 27 |
| | | | | Base Shear= 509 | Total OM= 63718 |

Table : 3.2 The calculation of overturning moment forearthquake load in xdirection in modal responsespectrum analysis method

| Level | Story Ht | Elev. | ETABS Cum. Story force/ Shear (Vx) | Individual Story Force/ Shear (Vx) | Overturning Moment (OM) |
|-------|-------------|-------|---|--|-------------------------------|
| ROOF | 10 | 160 | 21.438 | 21.438 | 3430.08 |
| F14 | 10 | 150 | 98.327 | 76.889 | 12302.24 |
| F13 | 10 | 140 | 169.273 | 70.946 | 10641.9 |
| F12 | 10 | 130 | 219.589 | 50.316 | 7044.24 |
| F11 | 10 | 120 | 256.572 | 36.983 | 4807.79 |
| F10 | 10 | 110 | 284.918 | 28.346 | 3401.52 |
| F9 | 10 | 100 | 307.599 | 22.681 | 2494.91 |
| F8 | 10 | 90 | 327.239 | 19.64 | 1964 |
| F7 | 10 | 80 | 346.589 | 19.35 | 1741.5 |
| F6 | 10 | 70 | 368.074 | 21.485 | 1718.8 |
| F5 | 10 | 60 | 392.315 | 24.241 | 1696.87 |
| F4 | 10 | 50 | 418.372 | 26.057 | 1563.42 |
| F3 | 10 | 40 | 444.605 | 26.233 | 1311.65 |
| F2 | 10 | 30 | 469.632 | 25.027 | 1001.08 |
| F1 | 10 | 20 | 495.992 | 26.36 | 790.8 |
| GF | 10 | 10 | 515.853 | 19.861 | 397.22 |
| | | | | Base Shear | Total OM |
| | | | | = 516 | = 56308 |

Table3.3: The calculation of overturning moment forearthquake load

in Y direction in equivalent lateral force method

| Level | Story Ht | Elev. | ETABS Cum. Story Force /Shear (Vy) | Indivitual Story Force /Shear (Vy) | Overturning Moment (OM) |
|-------|-------------|-------|---|--|-------------------------------|
| ROOF | 10 | 160 | 58.641 | 58.641 | 9382.56 |
| F14 | 10 | 150 | 128.141 | 69.5 | 11120 |
| F13 | 10 | 140 | 190.722 | 62.581 | 9387.15 |
| F12 | 10 | 130 | 246.636 | 55.914 | 7827.96 |
| F11 | 10 | 120 | 296.145 | 49.509 | 6436.17 |
| F10 | 10 | 110 | 339.52 | 43.375 | 5205 |
| F9 | 10 | 100 | 377.046 | 37.526 | 4127.86 |
| F8 | 10 | 90 | 409.018 | 31.972 | 3197.2 |
| F7 | 10 | 80 | 435.75 | 26.732 | 2405.88 |
| F6 | 10 | 70 | 457.571 | 21.821 | 1745.68 |
| F5 | 10 | 60 | 474.834 | 17.263 | 1208.41 |
| F4 | 10 | 50 | 487.918 | 13.084 | 785.04 |
| F3 | 10 | 40 | 497.239 | 9.321 | 466.05 |
| F2 | 10 | 30 | 504.296 | 7.057 | 282.28 |
| F1 | 10 | 20 | 508.102 | 3.806 | 114.18 |
| GF | 10 | 10 | 509.452 | 1.35 | 27 |
| | | | | Base Shear = 509 | Total OM = 63718 |

Table : 3.4 The calculation of overturning moment for earthquake load in Y direction in modal response spectrum analysis method

| Level | Story Ht | Elev. | ETABS Cum. Story Force/ Shear (Vy) | Indivitual Story Force/Shear (Vy) | Overturning Moment (OM) |
|-------|-------------|-------|---|--|-------------------------------|
| ROOF | 10 | 160 | 17.61 | 17.61 | 2817.6 |
| F14 | 10 | 150 | 84.88 | 67.27 | 10763.2 |
| F13 | 10 | 140 | 157.717 | 72.837 | 10925.55 |
| F12 | 10 | 130 | 215.638 | 57.921 | 8108.94 |
| F11 | 10 | 120 | 260.382 | 44.744 | 5816.72 |
| F10 | 10 | 110 | 294.161 | 33.779 | 4053.48 |
| F9 | 10 | 100 | 319.567 | 25.406 | 2794.66 |
| F8 | 10 | 90 | 339.365 | 19.798 | 1979.8 |
| F7 | 10 | 80 | 356.345 | 16.98 | 1528.2 |
| F6 | 10 | 70 | 373.198 | 16.853 | 1348.24 |
| F5 | 10 | 60 | 392.049 | 18.851 | 1319.57 |
| F4 | 10 | 50 | 413.953 | 21.904 | 1314.24 |
| F3 | 10 | 40 | 438.725 | 24.772 | 1238.6 |
| F2 | 10 | 30 | 464.924 | 26.199 | 1047.96 |
| F1 | 10 | 20 | 494.811 | 29.887 | 896.61 |
| GF | 10 | 10 | 519.267 | 24.456 | 489.12 |
| | | | | Base Shear = 519 | Total OM = 56442 |

From the above tables it observed that the overturning moments are higher in both direction in equivalent lateral force method than response spectrum method. Overturning moment in top floor is high cause the story shear is high and multiply with highest distance from bottom to top for equivalent lateral force method while in response spectrum method the story shear is so less.

From figure 3.1and 3.2 it shown that overall overturning moment in equivalent lateral force method is 11.63% greater than the response spectrum method in X direction and 11.42% in Y direction.

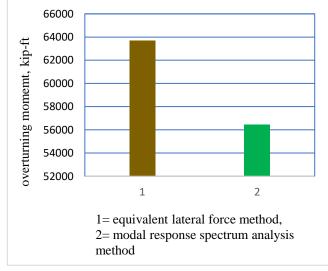
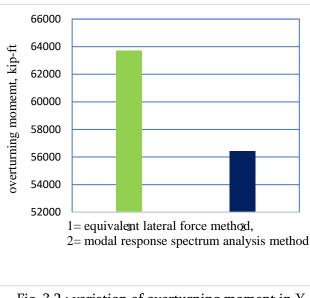
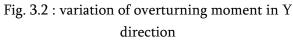


Fig. 3.1: variation of overturning moment in X direction





The eccentricity between the centre of mass and the geometric centroid of the building at that level shall not exceed 15% of the overall building width along each principal axis considered at each level [4]. In table 3.5 and table 3.6 eccentricity calculations are shown.

Table3.5:The calculation of eccentricity inequivalent lateral force method

| 64 | C.M | | C.R | | Eccentricity | |
|-------|---------|---------|-------|-------|--------------|------|
| Story | Xm | Уm | XCR | YCR | ex | ey |
| ROOF | 18.6198 | 41.5682 | 19.80 | 38.58 | 1.18 | 2.99 |
| F14 | 17.0505 | 41.996 | 19.73 | 38.61 | 2.68 | 3.39 |
| F13 | 17.0505 | 41.996 | 19.67 | 38.67 | 2.62 | 3.33 |
| F12 | 17.0505 | 41.996 | 19.61 | 38.73 | 2.55 | 3.26 |
| F11 | 17.0505 | 41.996 | 19.55 | 38.80 | 2.50 | 3.20 |
| F10 | 17.0505 | 41.996 | 19.49 | 38.85 | 2.44 | 3.15 |
| F9 | 17.0505 | 41.996 | 19.44 | 38.89 | 2.39 | 3.11 |
| F8 | 17.0505 | 41.996 | 19.38 | 38.92 | 2.33 | 3.08 |
| F7 | 17.0505 | 41.996 | 19.34 | 38.93 | 2.29 | 3.07 |
| F6 | 17.0505 | 41.996 | 19.29 | 38.91 | 2.24 | 3.09 |
| F5 | 17.0505 | 41.996 | 19.24 | 38.87 | 2.19 | 3.13 |
| F4 | 17.0505 | 41.996 | 19.20 | 38.79 | 2.15 | 3.21 |
| F3 | 17.0505 | 41.996 | 19.15 | 38.67 | 2.10 | 3.33 |
| F2 | 16.9067 | 42.1302 | 19.08 | 38.49 | 2.17 | 3.64 |
| F1 | 16.9027 | 42.1098 | 18.96 | 38.33 | 2.06 | 3.78 |
| GF | 16.9805 | 42.2318 | 18.67 | 37.94 | 1.69 | 4.29 |

Table 3.6: The calculation of eccentricity in modal response spectrum method

| Story | C.M | | C | .R | Ec | centricity |
|-------|---------|---------|-------|-------|------|------------|
| | Xm | Уm | XCR | YCR | ex | ey |
| ROOF | 18.6198 | 41.5682 | 19.86 | 38.47 | 1.24 | 3.10 |
| F14 | 17.0505 | 41.996 | 19.79 | 38.50 | 2.74 | 3.49 |
| F13 | 17.0505 | 41.996 | 19.73 | 38.56 | 2.68 | 3.43 |
| F12 | 17.0505 | 41.996 | 19.68 | 38.63 | 2.63 | 3.37 |
| F11 | 17.0505 | 41.996 | 19.62 | 38.69 | 2.57 | 3.31 |
| F10 | 17.0505 | 41.996 | 19.57 | 38.75 | 2.52 | 3.25 |
| F9 | 17.0505 | 41.996 | 19.51 | 38.79 | 2.46 | 3.20 |
| F8 | 17.0505 | 41.996 | 19.46 | 38.82 | 2.41 | 3.17 |
| F7 | 17.0505 | 41.996 | 19.41 | 38.84 | 2.36 | 3.16 |
| F6 | 17.0505 | 41.996 | 19.36 | 38.83 | 2.31 | 3.16 |
| F5 | 17.0505 | 41.996 | 19.31 | 38.80 | 2.26 | 3.20 |
| F4 | 17.0505 | 41.996 | 19.26 | 38.73 | 2.21 | 3.27 |
| F3 | 17.0505 | 41.996 | 19.21 | 38.62 | 2.15 | 3.37 |
| F2 | 16.9067 | 42.1302 | 19.12 | 38.46 | 2.22 | 3.67 |
| F1 | 16.9027 | 42.1098 | 18.99 | 38.31 | 2.09 | 3.80 |
| GF | 16.9805 | 42.2318 | 18.69 | 37.93 | 1.71 | 4.30 |

From the table 3.7 and table 3.8 it shown that the eccentricity value increased 2.7% average in modal response spectrum method than equivalent lateral force method in X direction and 2.28% in Y direction.

Table 3.7: percent difference in eccentricity in X direction

| Level | e _x , equivalent lateral force method | e _x , modal response spectrum method | % Difference |
|-------|---|---|--------------|
| ROOF | 1.18 | 1.24 | 4.83871 |
| F14 | 2.68 | 2.74 | 2.189781 |
| F13 | 2.62 | 2.68 | 2.238806 |
| F12 | 2.55 | 2.63 | 3.041825 |
| F11 | 2.5 | 2.57 | 2.723735 |
| F10 | 2.44 | 2.52 | 3.174603 |
| F9 | 2.39 | 2.46 | 2.845528 |
| F8 | 2.33 | 2.41 | 3.319502 |
| F7 | 2.29 | 2.36 | 2.966102 |
| F6 | 2.24 | 2.31 | 3.030303 |
| F5 | 2.19 | 2.26 | 3.097345 |
| F4 | 2.15 | 2.21 | 2.714932 |
| F3 | 2.1 | 2.15 | 2.325581 |
| F2 | 2.17 | 2.22 | 2.252252 |
| F1 | 2.06 | 2.09 | 1.435407 |
| GF | 1.69 | 1.71 | 1.169591 |

Table 3.8: percent difference in eccentricity in Y direction

| level | ey, equivalent lateral force method | ey, modal response spectrum method | % Difference |
|-------|---|---|--------------|
| ROOF | 2.99 | 3.1 | 3.548387 |
| F14 | 3.39 | 3.49 | 2.86533 |
| F13 | 3.33 | 3.43 | 2.915452 |
| F12 | 3.26 | 3.37 | 3.264095 |
| F11 | 3.2 | 3.31 | 3.323263 |
| F10 | 3.15 | 3.25 | 3.076923 |
| F9 | 3.11 | 3.2 | 2.8125 |
| F8 | 3.08 | 3.17 | 2.839117 |
| F7 | 3.07 | 3.16 | 2.848101 |
| F6 | 3.09 | 3.16 | 2.21519 |
| F5 | 3.13 | 3.2 | 2.1875 |
| F4 | 3.21 | 3.27 | 1.834862 |
| F3 | 3.33 | 3.37 | 1.186944 |
| F2 | 3.64 | 3.67 | 0.817439 |
| F1 | 3.78 | 3.8 | 0.526316 |
| GF | 4.29 | 4.3 | 0.232558 |

IV. CONCLUSION

Equivalent lateral force method gives higher value for overturning moment especially in high-rise building which is more conservative than response spectrum method. Equivalent lateral force method gives lower value for eccentricity than response spectrum method. High value of overturning moment is more important in I-shaped building for stability of the building. During earthquake response overturning moment affect the foundation of the building. However as for equivalent lateral force method is more conservative response spectrum method can be used for high rise building. Though eccentricity is greater in response spectrum method but the values are less difference in percentage in both analysis method.

Conclusion are based on findings of the study; further study should be done using different shape of building with plan irregularity and height. Also, torsional moment effect due to eccentricity should be studied in further.

V. REFERENCES

 Devikashree M L, B.S Jayashankara babu. 2017. A Study on Effect of Eccentricity in RC Frame Structures, International Journal of Innovative Research in Science, Engineering and



Technology, Vol. 6, Issue 6, June 2017, ISSN(Online): 2319-8753

- [2]. Atif Zakaria, M. Shiva Rama Krishna, T.G.N.C.Vamsi Krishna, Mirza Mahaboob Baig.
 2019. Effects of the Accidental Eccentricity on Regular and Irregular Buildings, International Journal of Innovative Technology and Exploring Engineering (IJITEE), Volume-8 Issue-11, September 2019, ISSN: 2278-3075
- [3]. BNBC (part 6, chapter 2) 2020, Bangladesh National Building Code, Bangladesh Government Press, Dhaka, Bangladesh.
- [4]. ASCE/SEI/7-16 (appendix D), Minimum Design Loads and Associated Criteria for Buildings and other Structures, American Society of Civil Engineers.

Cite this article as :

M. T. Hasan, M. L. Hossain, "Comparative Study on Overturning Moment and Eccentricity of A I-Shaped Building by Equivalent Lateral Force and Modal Response Spectrum Method Using ETABS Software", International Journal of Scientific Research in Science and Technology (IJSRST), Online ISSN : 2395-602X, Print ISSN : 2395-6011, Volume 8 Issue 4, pp. 173-179, July-August 2021. Available at doi : https://doi.org/10.32628/IJSRST218262 Journal URL : https://ijsrst.com/IJSRST218262